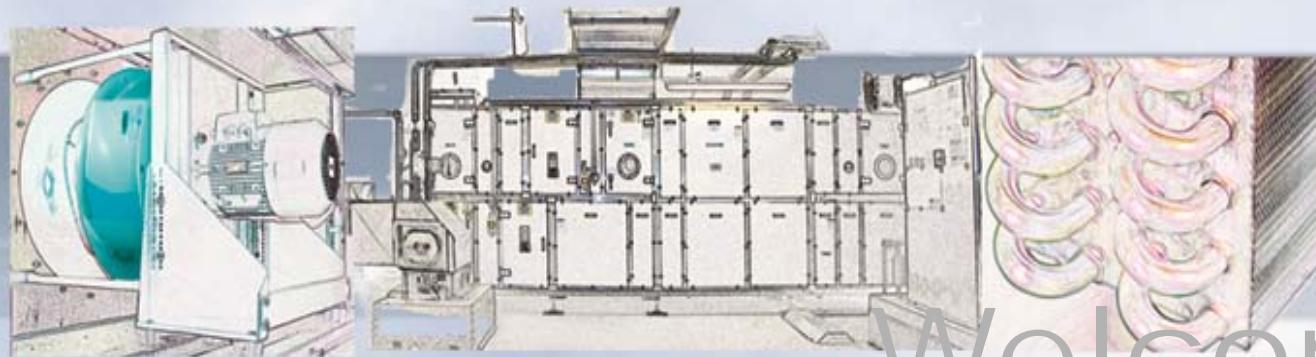


Willkommen



Welcome
Bienvenue

Ventilation energy efficiency of fans and drives Energy recovery and energy efficiency in ventilation technology

Prof. Dr.-Ing. Christoph Kaup
c.kaup@umwelt-campus.de

Ventilation systems tasks:

Thermodynamic air treatment

- Heating
- Cooling
- Humidification
- Dehumidification

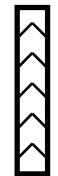


Ventilation systems tasks:

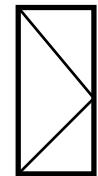
Thermodynamic air treatment

Example of a ventilation system (supply air)

WP



F



HRS



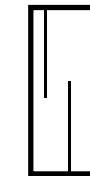
C



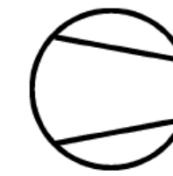
H



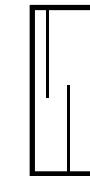
S



V



S



ODA

SUP



Ventilation systems tasks:

Transport of air

- fan
- motor
- drive
- control



Energy demand in ventilation systems

- Air treatment
 - heating/cooling/de-/humidification
- Air transport
 - against Δp internal/external



Power consumption

$$P_m = \dot{V} \cdot \Delta p \cdot 1 / \eta_s$$

P_m absorbed power consumption [KW]

\dot{V} air flow [m^3/s]

Δp pressure losses of the system [Pa]

η_s system efficiency [./.]



$$\eta_s = \eta_F \cdot \eta_M \cdot \eta_D \cdot \eta_C$$

fan • motor • drive • control



DIN EN 13779

Ventilation system non-residential
General requirements and measured values

$$P_{SFP} = \frac{P_{Input}}{q_v} = \frac{\Delta p_{fan}}{\eta_{total}}$$

P_{SFP}	specific fan power [W/(m ³ /s)]
P_{Input}	electric power consumption [W]
q_v	air flow rate [m ³ /s]
Δp_{fan}	total pressure [Pa]
η_{total}	system efficiency [-]



Specific Fan Power

EN 13779: 2007

category	P_{SFP} W/(m³/s)
SFP 1	≤ 500
SFP 2	≤ 750
SFP 3	≤ 1.250
SFP 4	≤ 2.000
SFP 5	≤ 3.000
SFP 6	≤ 4.500
SFP 7	> 4.500

Δp_{Fan} [Pa]	
$\eta_{total} 0,55$	$\eta_{total} 0,65$
275	325
410	485
685	810
1.100	1.300
1.650	1.950
2.475	2.925

application	default value
EXH without HR	SFP 2
EXH with HR	SFP 3
SUP without HR	SFP 3
SUP full AC	SFP 4

for specific components (e. g. HEPA-Filter, HRS H1 or H2) is a use of additional SFP possible.



Additional fan power

EN 13779: 2007

	component	add. P_{SFP} [W/(m³/s)]
1	add. filterstage	+ 300
2	HEPA filter	+ 1.000
3	gasfilter	+ 300
4	HRS class H2-H1	+ 300
5	high capacity cooler	+ 300



Air velocity classes

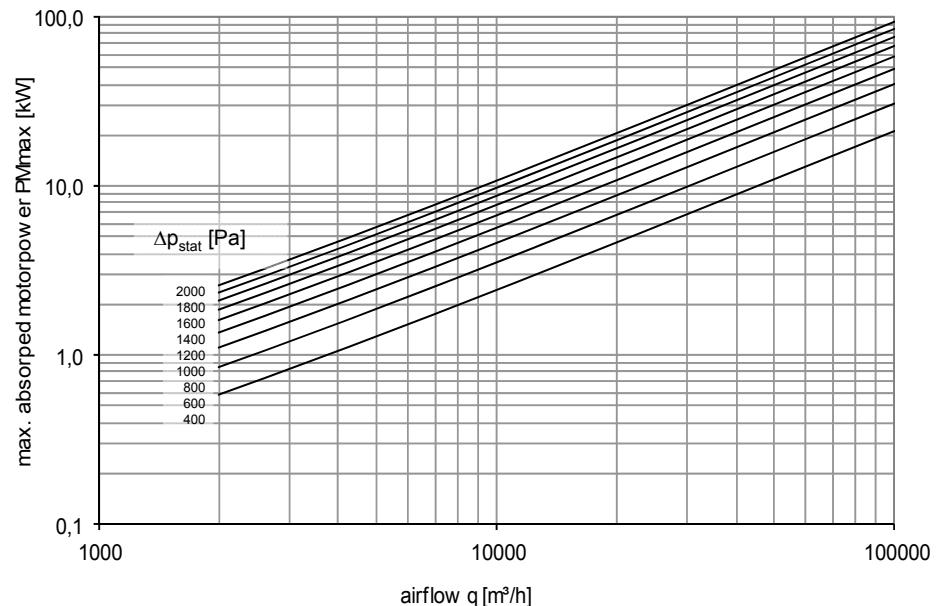
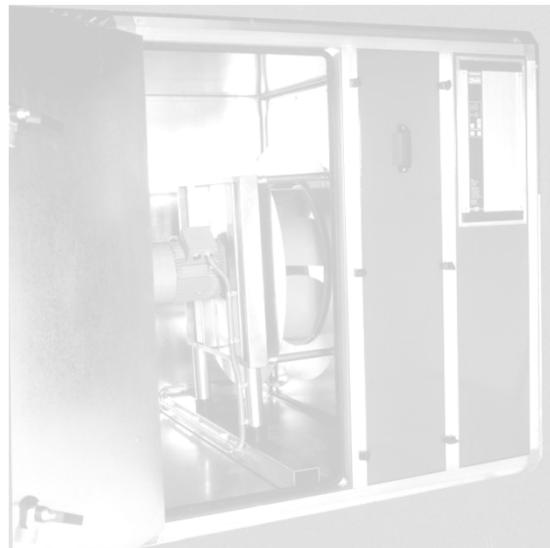
EN 13053: 2012

class	velocity in m/s
V1	$\leq 1,6 \text{ m/s}$
V2	$\leq 1,8 \text{ m/s}$
V3	$\leq 2,0 \text{ m/s}$
V4	$\leq 2,2 \text{ m/s}$
V5	$\leq 2,5 \text{ m/s}$
V6	$\leq 2,8 \text{ m/s}$
V7	$\leq 3,2 \text{ m/s}$
V8	$\leq 3,6 \text{ m/s}$
V9	$> 3,6 \text{ m/s}$

Electric power consumption fans



European Committee for Standardization
Comité Européen de Normalisation
Europäisches Komitee für Normung



$P_{\text{input max}}$	(kW)
Δp_{stat}	(Pa)
q_v	(m^3/s)

class	equation
Base	$P_{\text{Input max}} = \left(\frac{\Delta p_{\text{stat.}}}{450} \right)^{0,925} \times \left(q_v + 0,08 \right)^{0,95}$

Power consumption classes

EN 13053: 2012

class	powerconsumption related to Pm_{ref}
P1	$\leq Pm_{ref} \cdot 0.85$
P2	$\leq Pm_{ref} \cdot 0.90$
P3	$\leq Pm_{ref} \cdot 0.95$
P4	$\leq Pm_{ref} \cdot 1.00$
P5	$\leq Pm_{ref} \cdot 1.06$
P6	$\leq Pm_{ref} \cdot 1.12$
P7	$> Pm_{ref} \cdot 1.12$

Energy efficiency

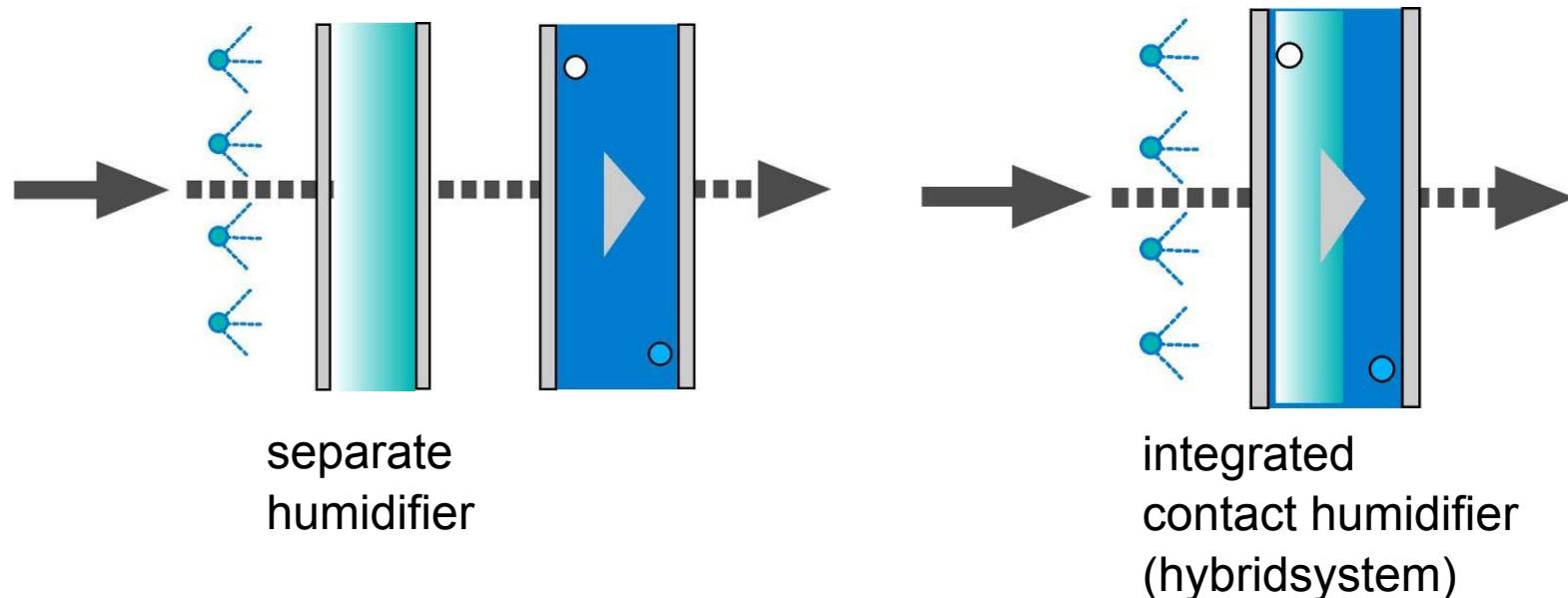
- reduction of components (e. g. drop eliminator)
- hybrid components (humidifier)
- bypasses in components



Energy efficiency

Internal pressure losses

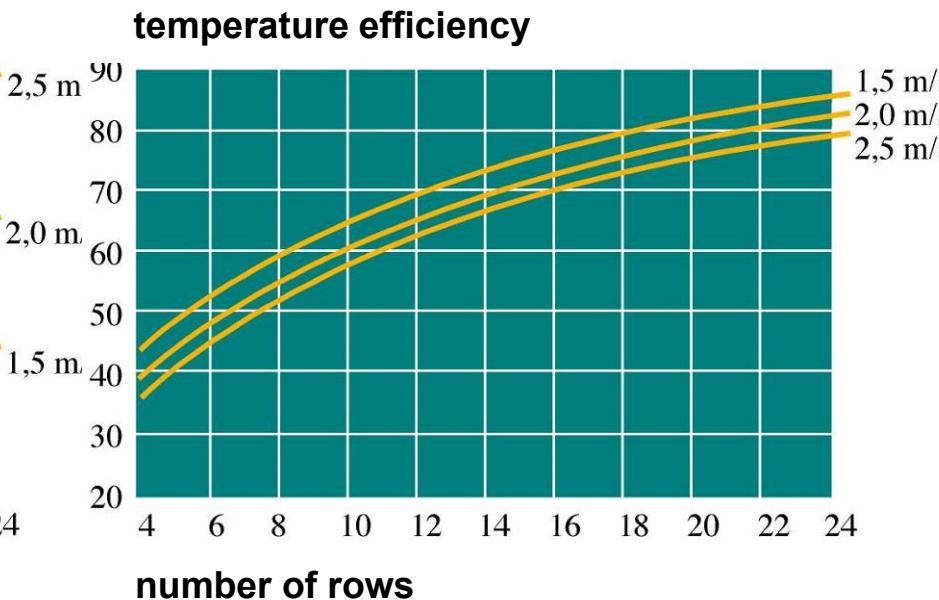
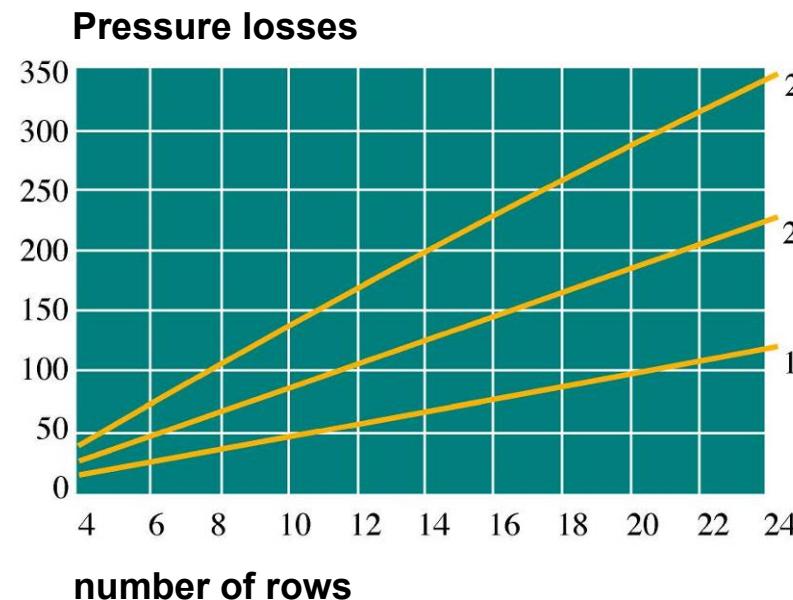
components (example hybrid humidifier)



Energy efficiency

Internal pressure losses

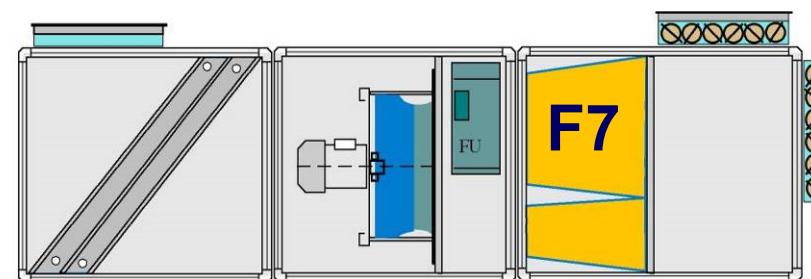
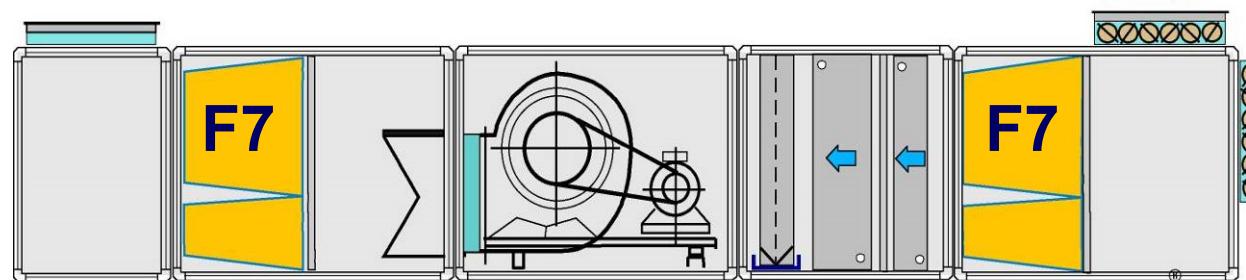
face velocity (example HRS – CC-System)



Energy efficiency

Internal pressure losses

arrangement of components



Filter stages

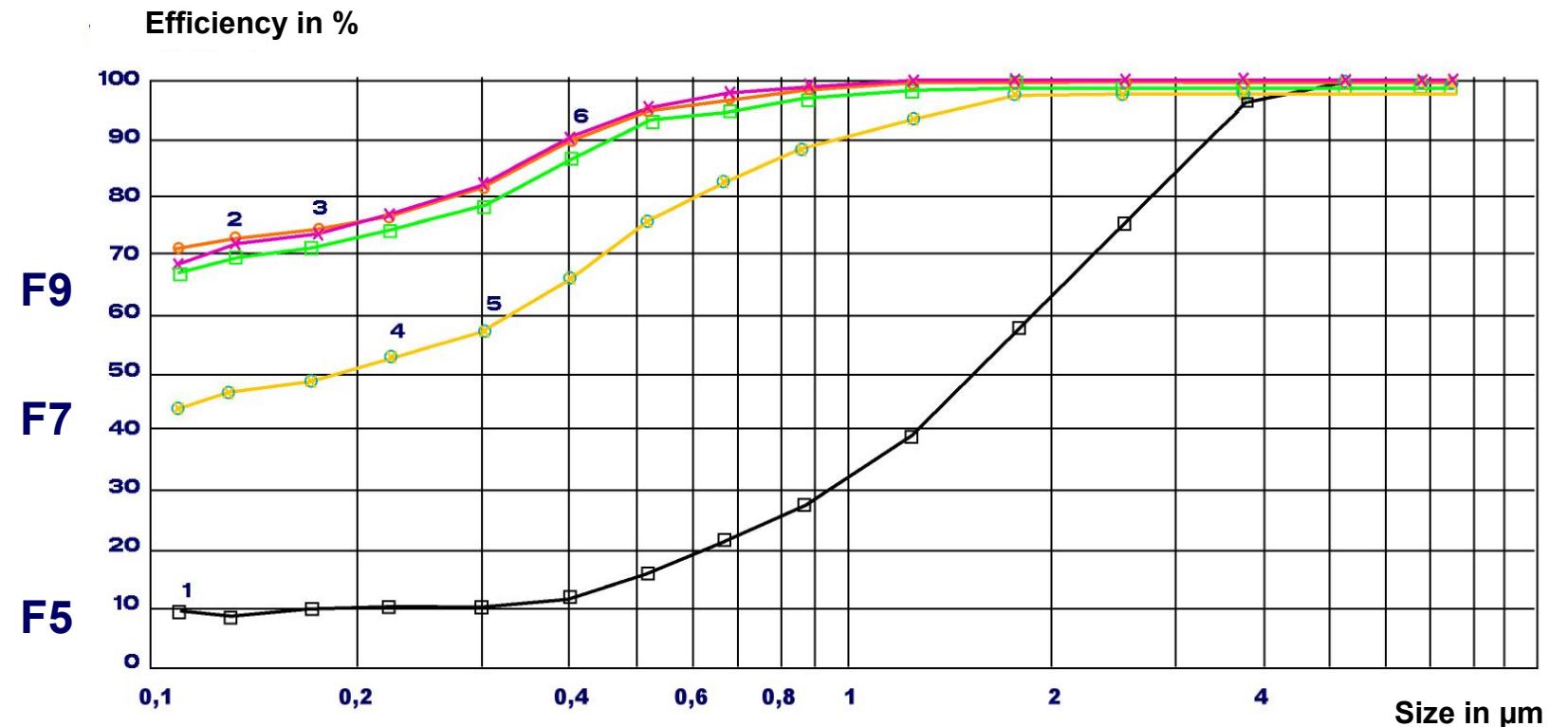
Single stage

- first stage F7 (80 % at 1 µm)
- better protection of the AHU
- reduction of pressure losses
- reduction of AHU lenght

Two filter stages

- first stage F7 (80 % at 1 µm)
- second stage F7 = efficiency (F5 / F9)
- reduction of pressure losses

AHU components



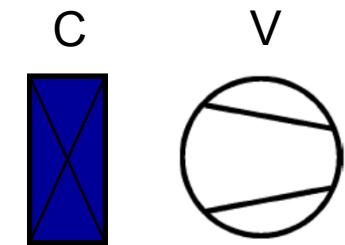
F5 + F9 4,5 m^2 F5 55 Pa 200 Pa 3.400 m^3/h 450 Pa
 9,0 m^2 F9 140 Pa 250 Pa 3.400 m^3/h

F7 + F7 9,0 m^2 F7 95 Pa 150 Pa 3.400 m^3/h 260 Pa
 9,0 m^2 F7 95 Pa 110 Pa 3.400 m^3/h

Cooler

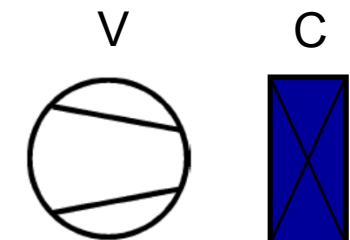
Suction side

- use with dehumidification
- fan waste heat used to reheat
- fin space e. g. 2,5 mm



Pressure side

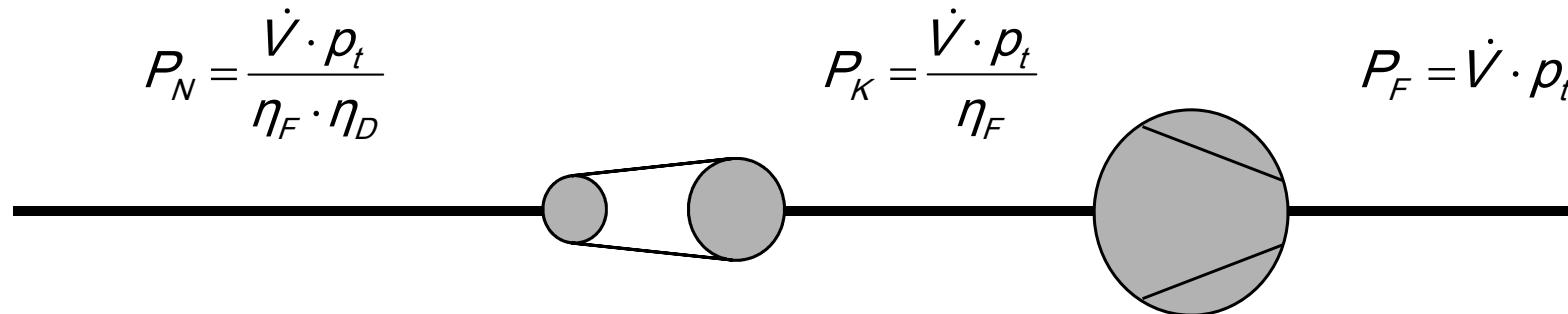
- use with a „dry“ cooling
- fan waste heat before the cooler
- bigger average log. temperature difference



Air transport

Power

mechanical



electrical

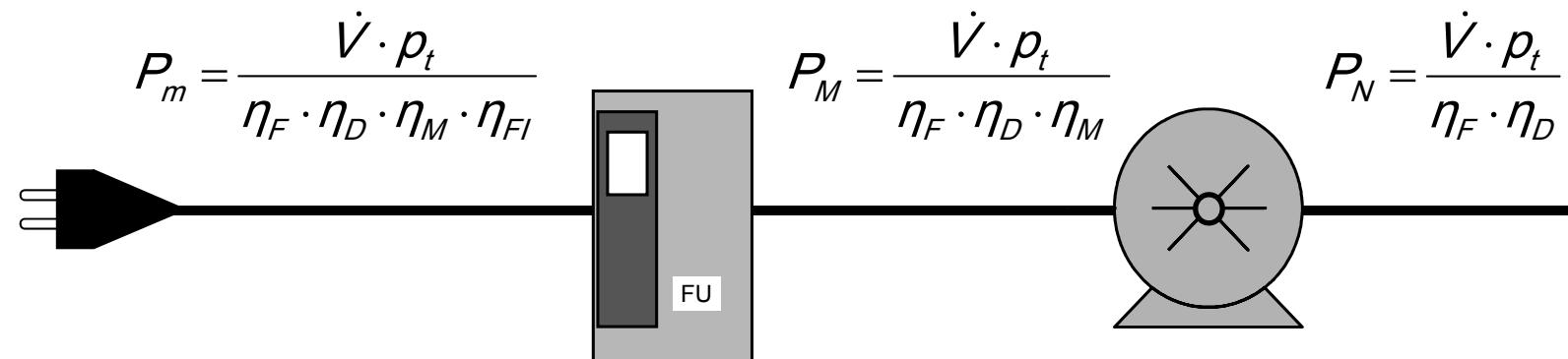
$$P_N = U \cdot I \cdot \sqrt{3} \cdot \cos \varphi \cdot \eta_{FI} \cdot \eta_M$$

$$P_K = U \cdot I \cdot \sqrt{3} \cdot \cos \varphi \cdot \eta_{FI} \cdot \eta_M \cdot \eta_D$$

$$P_V = U \cdot I \cdot \sqrt{3} \cdot \cos \varphi \cdot \eta_{FI} \cdot \eta_M \cdot \eta_D \cdot \eta_F$$

Air transport

Power
mechanical



electrical

$$P_m = U \cdot I \cdot \sqrt{3} \cdot \cos$$

Motor:

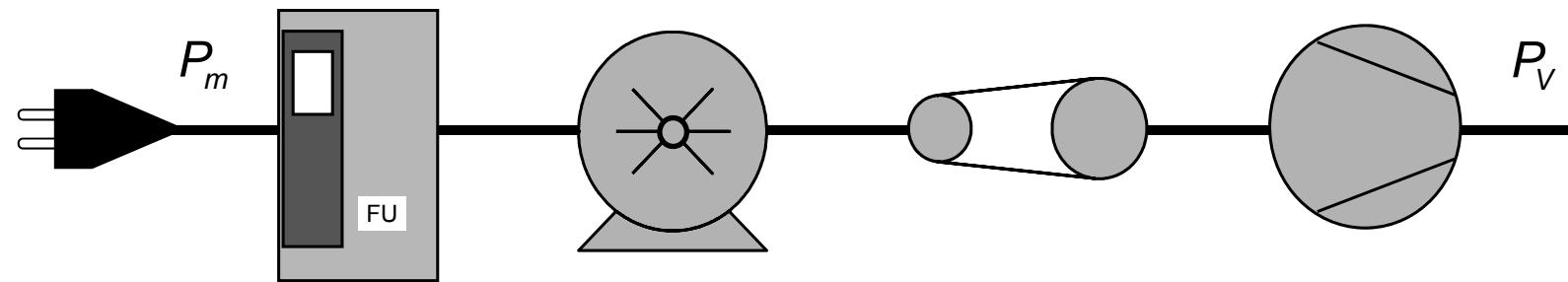
$$P_M = U \cdot I \cdot \sqrt{3} \cdot \cos \cdot \eta_{FI}$$

$$P_N = U \cdot I \cdot \sqrt{3} \cdot \cos \cdot \eta_{FI} \cdot \eta_M$$

Air transport

Power

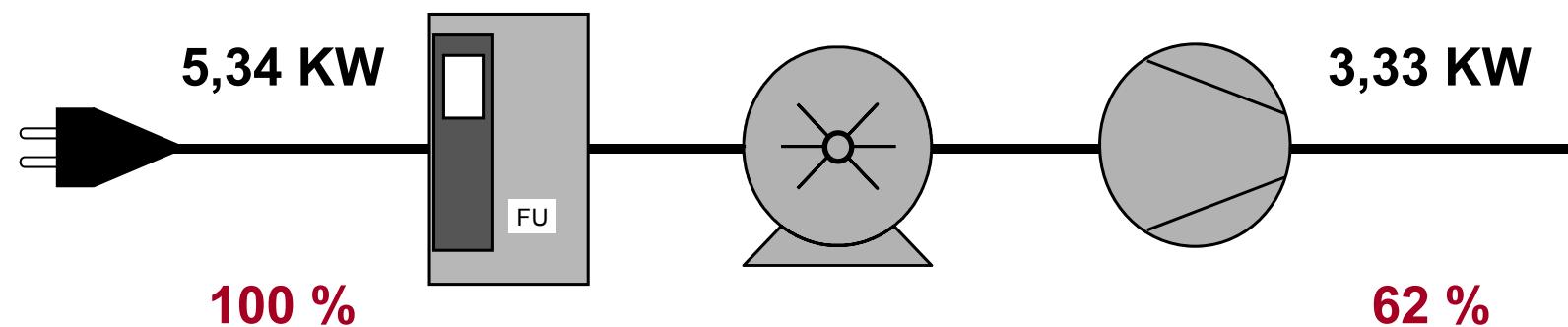
Systemefficiency η_{Syst}



$$\eta_{FI} \cdot \eta_M \cdot \eta_F \cdot \eta_D = \frac{P_V}{P_m} = \eta_{Syst}$$

Air transport

Example:



Air transport

Fan

Types

Axial with or
without a casing



Radial with
a casing



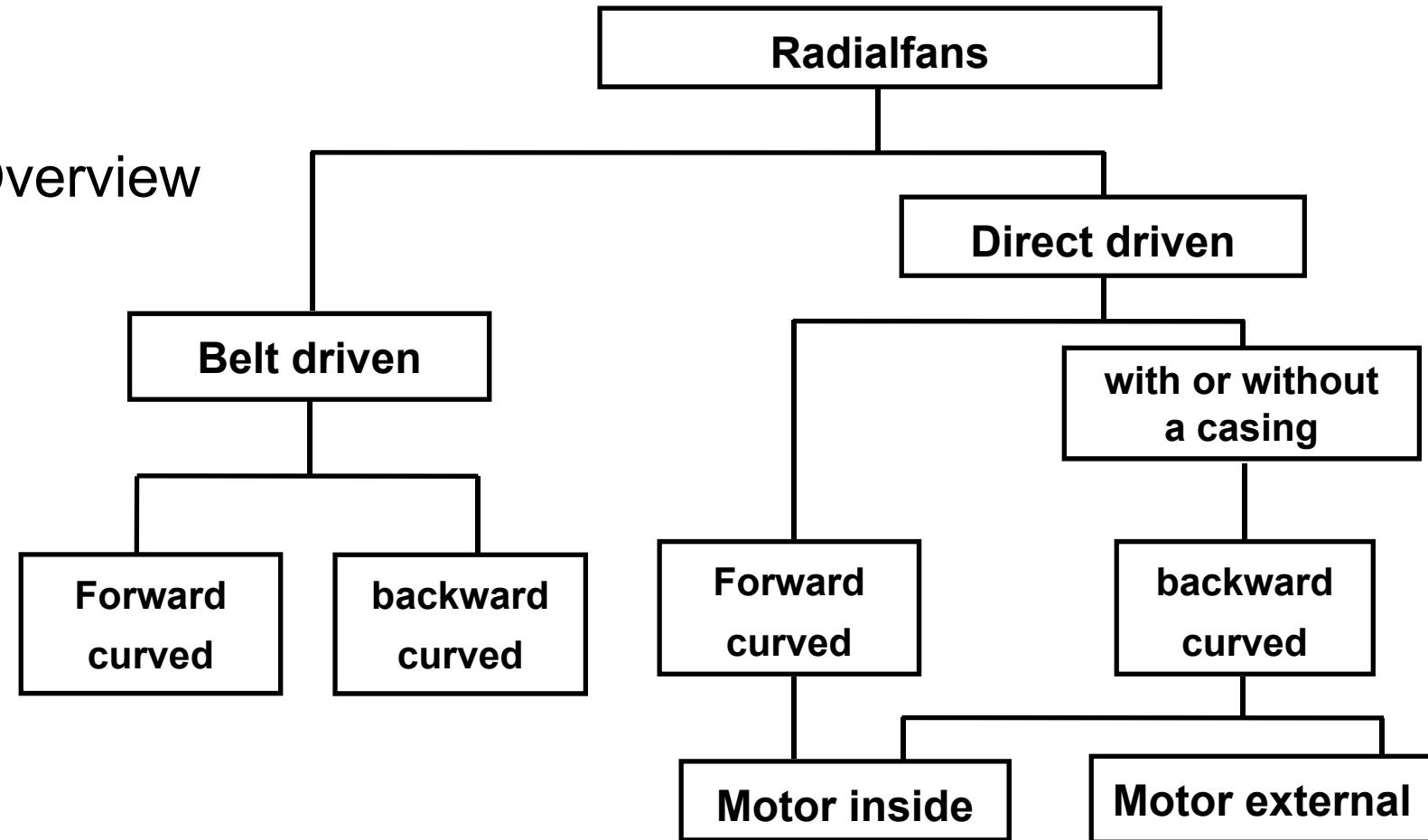
Radial without
a casing



Air transport

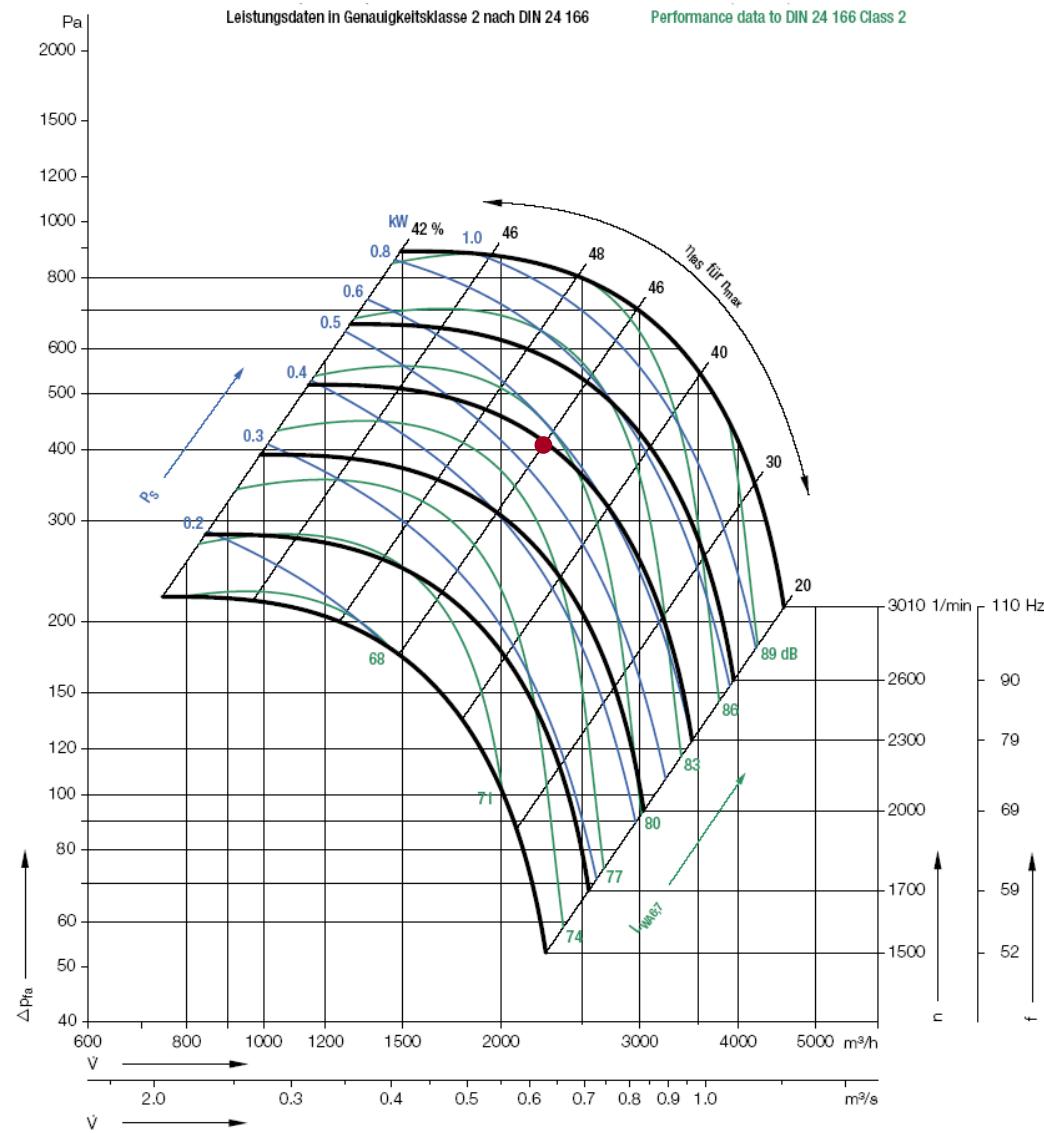
Fan

Overview



Air transport

Fan
Selection
characteristics



Fan concepts

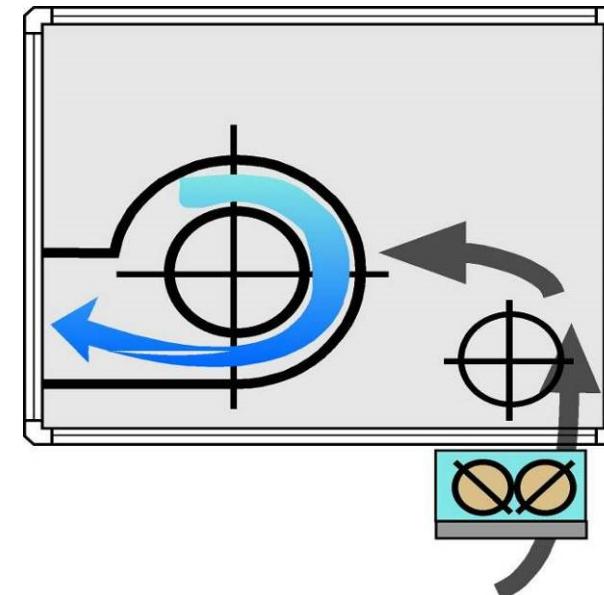
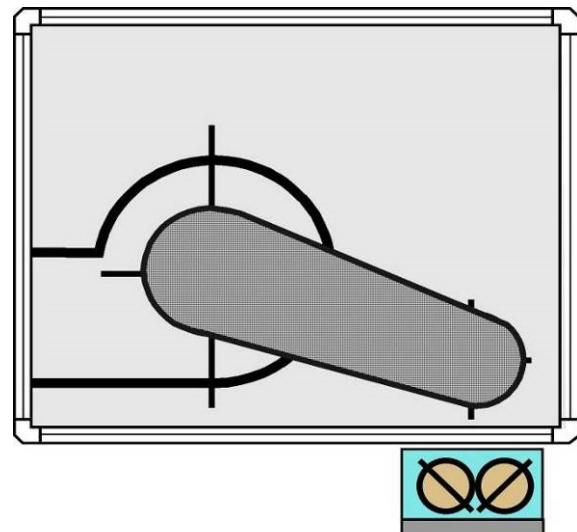


Energy efficiency

Internal pressure losses

inlet losses (example fan with a spiral housing)

$$\sum \Delta p_{EV} = 1,5 - 4,5 \cdot p_{dyn}$$

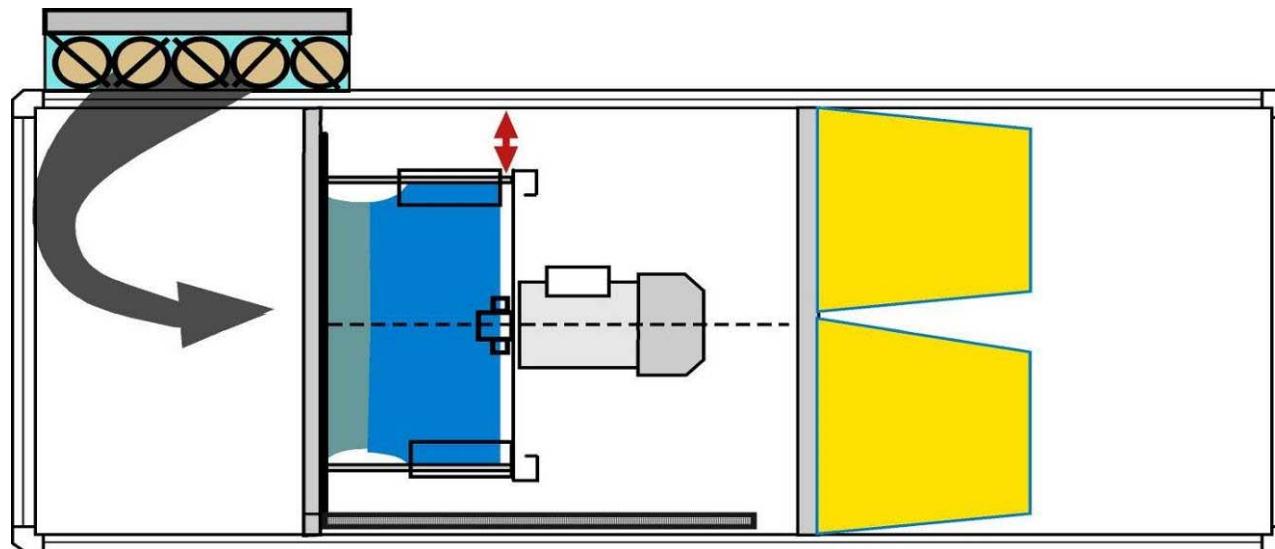


Energy efficiency

Internal pressure losses

inlet losses (example plugged fan without a housing)

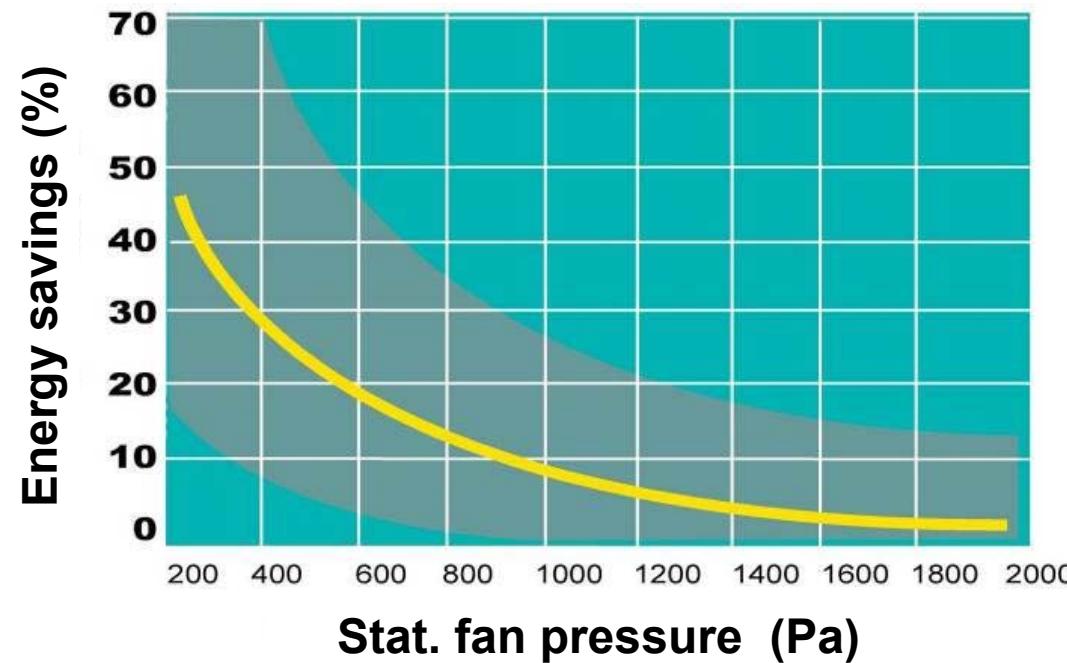
$$\sum \Delta p_{EV} = 0,5 - 1,5 \cdot p_{dyn}$$



Energy efficiency

Internal pressure losses

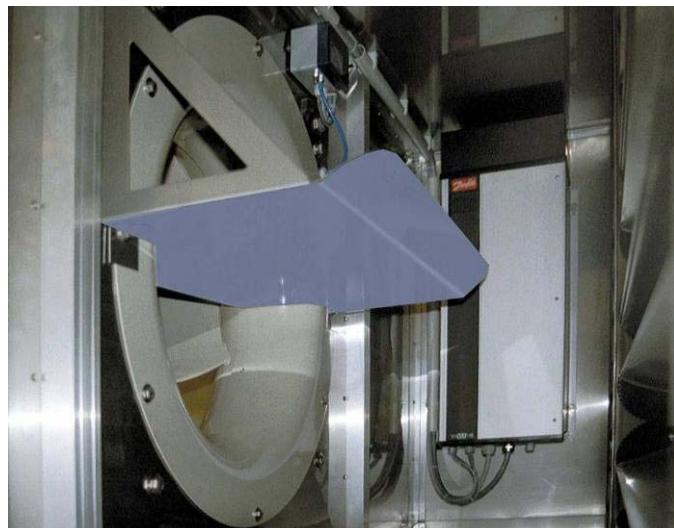
potential of plugged fans compared to spiral fans



Energy efficiency

Internal pressure losses

guide vane at a axial inlet situation



efficiency \blacktriangleleft turbulence \triangleright

DE 101 21 940

Air transport

Internal pressure losses

practice:

10.000 m³/h transported in a AHU against
a stat. pressure of $p_{stat} = 1.171 \text{ Pa}$



given: $\eta_{vt} = 80,5\%$; belt drive

impeller diameter $D = 400 \text{ mm}$
outlet area $501 \cdot 501 \text{ mm}$

$$\eta_M = 88,3\%$$

$$\eta_B = 94,0\%$$

$$\sum \Delta p_{EV} = 3,0 \cdot p_{dyn}$$

asked: motor power P_N

Air transport

Internal pressure losses

solution:



$$A_R = 0,501 \cdot 0,501 = 0,251 \text{ m}^2$$

$$w_{\text{fan outlet}} = 10.000 / 3.600 / A_R = 11,07 \text{ m/s}$$

$$p_{\text{dyn}} = \rho / 2 \cdot w^2 = 0,6 \cdot 11,07^2 = 74 \text{ Pa}$$

$$\Delta p_{EV} = 3 \cdot 74 = 222 \text{ Pa}$$

$$p_t = p_{\text{stat}} + \Delta p_{EV} = 1.171 + 222 = 1.393 \text{ Pa}$$

$$P_N = \dot{V} \cdot p_t / (\eta_{vt} \cdot \eta_K) = 10.000 / 3.600 \cdot 1.393 / (0,805 \cdot 0,94)$$
$$= \underline{\underline{5,113 \text{ KW}}}$$

Air transport

Power

given:

10.000 m³/h in a AHU against a pressure drop of
 $p_t = 1.200 \text{ Pa}$.



$\eta_{Ffa} = 71,0\%$; direct driven

Impeller diameter $D = 630 \text{ mm}$

Impeller width $b = 201 \text{ mm}$

$\eta_M = 88,3\%$

$\eta_{FI} = 97,0\%$

calculate:

Motorpower

P_N

Systemeff.

$\eta_{Syst.}$

absorpt motor power

P_m

Air transport

Power

solution:



$$A_R = D \cdot \pi \cdot b = 0,3978 \text{ m}^2$$

$$w_{\text{Impeller}} = 10.000 / 3.600 / A_R = 6,98 \text{ m/s}$$

$$p_{\text{dyn}} = \rho / 2 \cdot w^2 = 0,6 \cdot 6,98^2 = 29 \text{ Pa}$$

$$p_{\text{stat}} = 1.200 - 29 = 1.171 \text{ Pa}$$

$$P_N = \dot{V} \cdot p_{\text{stat}} / \eta_{\text{fa}} = \underline{\underline{4,581 \text{ KW}}} ; \text{ chosen motor } 5,5 \text{ KW}$$

$$\eta_t = \dot{V} \cdot p_t / P_N = 72,8 \%$$

$$\eta_{\text{Syst.}} = \eta_M \cdot \eta_t \cdot \eta_{\text{Fl}} = 0,883 \cdot 0,728 \cdot 0,97 = \underline{\underline{62,4 \%}}$$

$$P_m = p \cdot \dot{V} / \eta_{\text{Syst.}} = 1.200 \cdot 10.000 / 3.600 / 0,624 = \underline{\underline{5,342 \text{ KW}}}$$

Air transport

Internal pressure losses

solution:



$$A_R = D \cdot \pi \cdot b = 0,3978 \text{ m}^2$$

$$W_{\text{fan outlet}} = 10.000 / 3.600 / A_R = 6,98 \text{ m/s}$$

$$p_{\text{dyn}} = \rho / 2 \cdot w^2 = 0,6 \cdot 6,98^2 = 29 \text{ Pa}$$

$$p_{\text{stat}} = 1.200 - 29 = 1.171 \text{ Pa}$$

$$P_N = \dot{V} \cdot p_{\text{stat}} / \eta_{fa} = \underline{\underline{4,581 \text{ KW}}}$$

choose motor 5,5 KW

Air transport

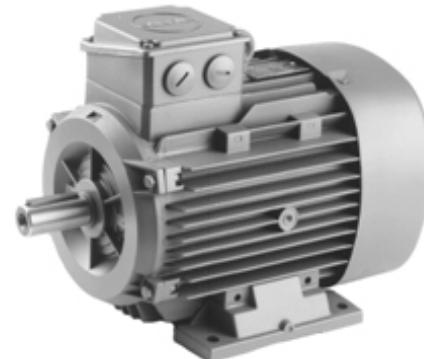
Motor

Types

AC
Rotary current
with 3 phases
alternating current

EC
electric
commutated
continuous current

PM
permanent
magnet Motor



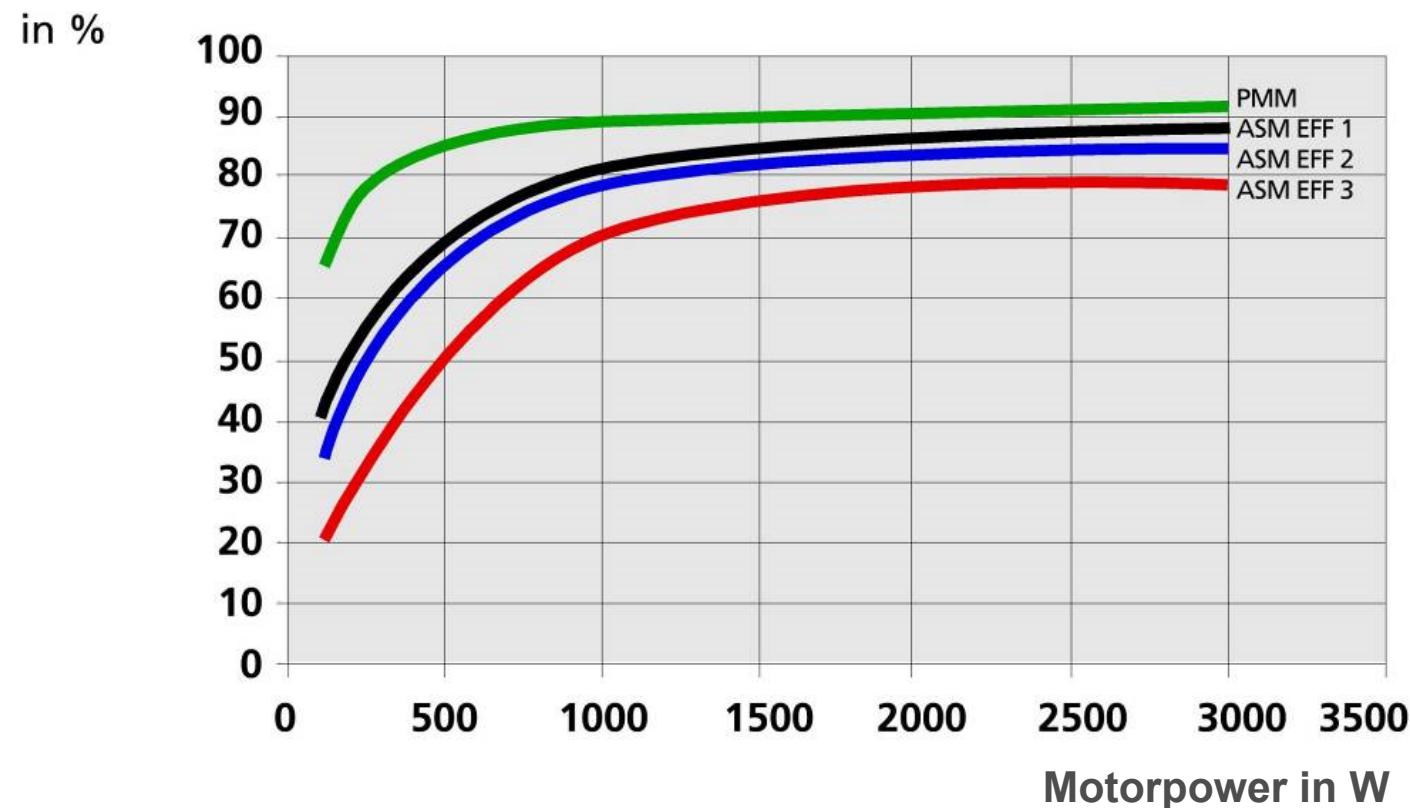
Air transport

Motor

Efficiencies (example n = 1.500 1/min)

Power	IE2	IE3
1,1 KW	77,0 %	84,0 %
2,2 KW	82,0 %	86,5 %
4,0 KW	85,0 %	88,5 %
7,5 KW	87,0 %	90,3 %
55,0 KW	93,5 %	95,1 %

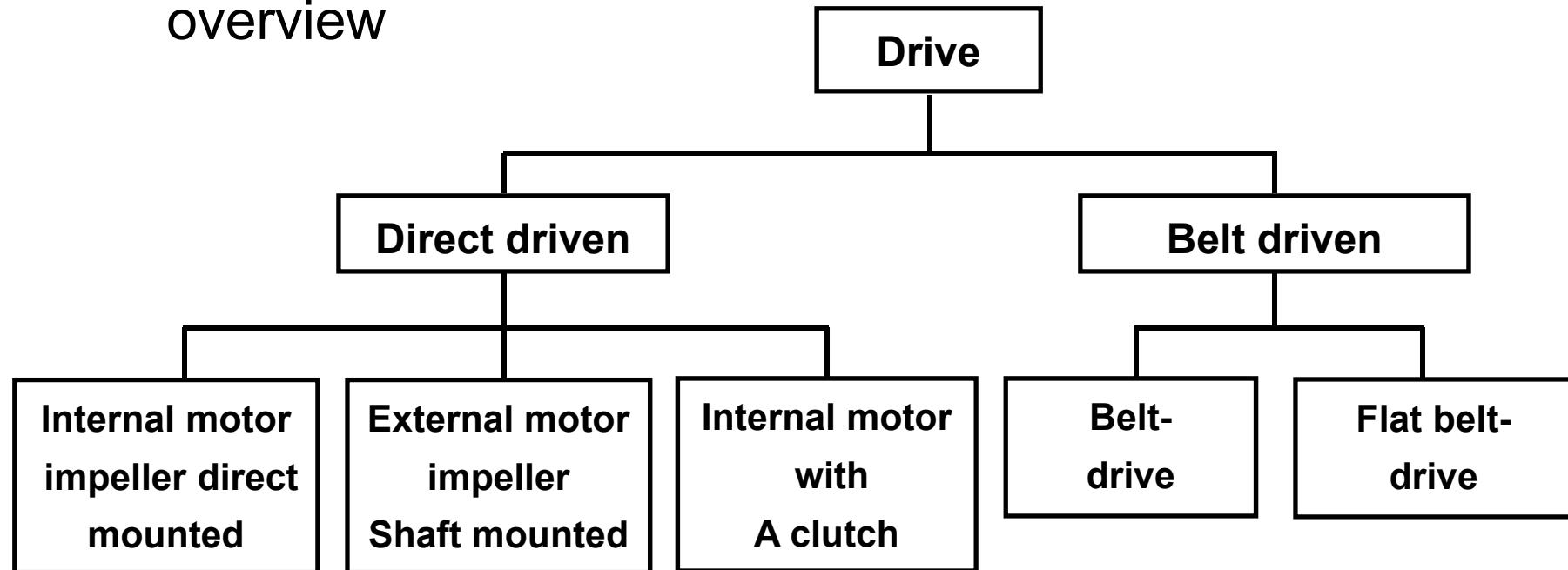
Motors



Air transport

Drive

Coupling fan / motor
overview



Air transport

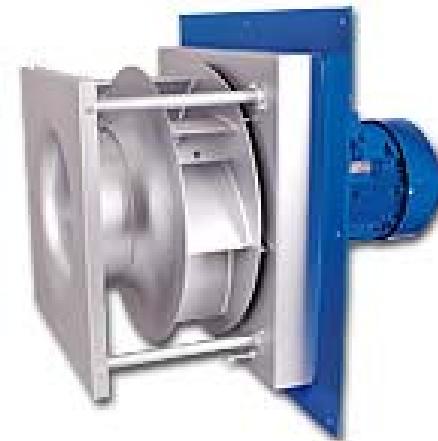
Drive

Coupling fan / motor

indirect
via belt
(standard or flat belt)



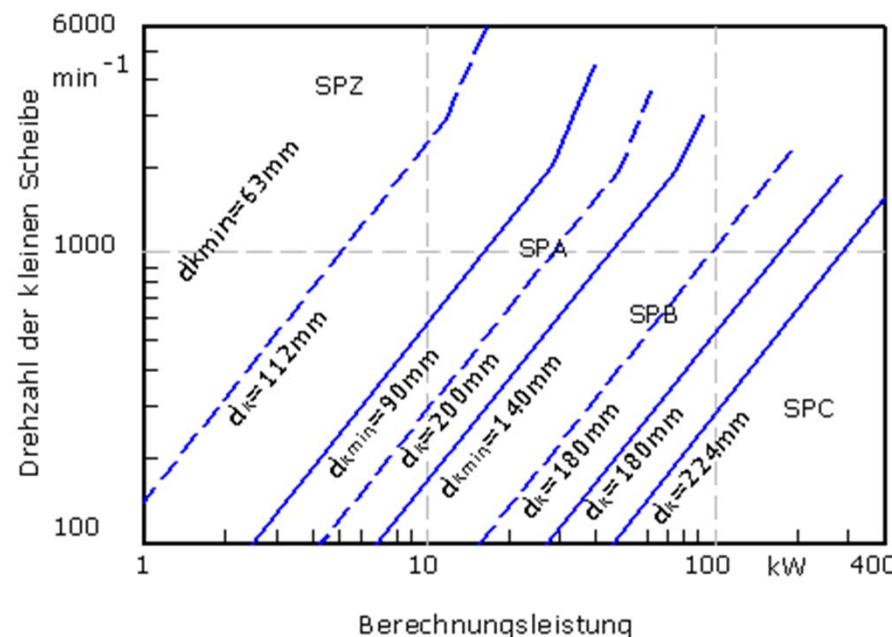
direct



Air transport

Drive

Coupling fan / motor



Waste power:

standard belt
3 – 12 %

flat belt
2 – 4 %

Air transport

Control

Air flow

speed control

e. g. via
frequency inverter



**power
losses:**

3 – 5 %

pressure control

e. g. via
dampers



Energy efficiency

Proportional law

Air flow

$$\frac{\dot{V}_2}{\dot{V}_1} = \frac{n_2}{n_1}$$

Pressure

$$\left(\frac{\dot{V}_2}{\dot{V}_1}\right)^2 = \frac{\Delta p_2}{\Delta p_1}$$

Power consumption

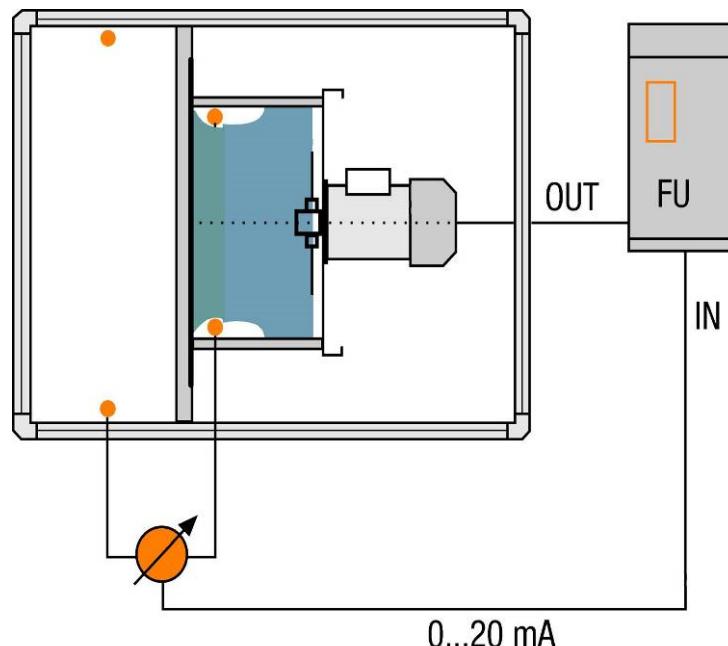
$$\left(\frac{\dot{V}_1}{\dot{V}_2}\right)^3 = \frac{P_1}{P_2}$$

Energy efficiency

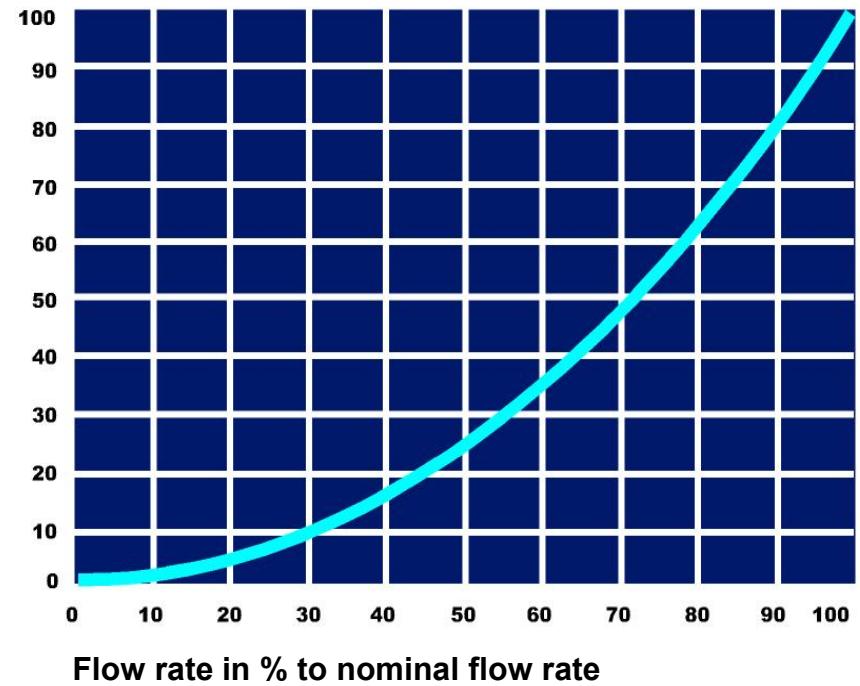
Air flow rate-measuring device

effective pressure to air flow

$$\dot{V} = \alpha \cdot \varepsilon \cdot \frac{d^2 \cdot \pi}{4} \cdot \sqrt{\frac{2 \cdot \Delta p}{\rho}}$$



Eff. pressure in % to nominal pressure



Energy efficiency

Proportional law

given:

$\dot{V}_1 = 10.000 \text{ m}^3/\text{h}$ transported with a air handling unit against
 $p_{t1} = 1.200 \text{ Pa}$ with a speed of $n_1 = 1.783 \text{ min}^{-1}$.
The absorbed motor power is $Pm_1 = 5,7 \text{ KW}$.

calculate:

Parameter p_{t2} , n_2 , Pm_2
at a reduced air flow of 80%

($\dot{V}_2 = 8.000 \text{ m}^3 / \text{h}$).

Energy efficiency

Proportional law

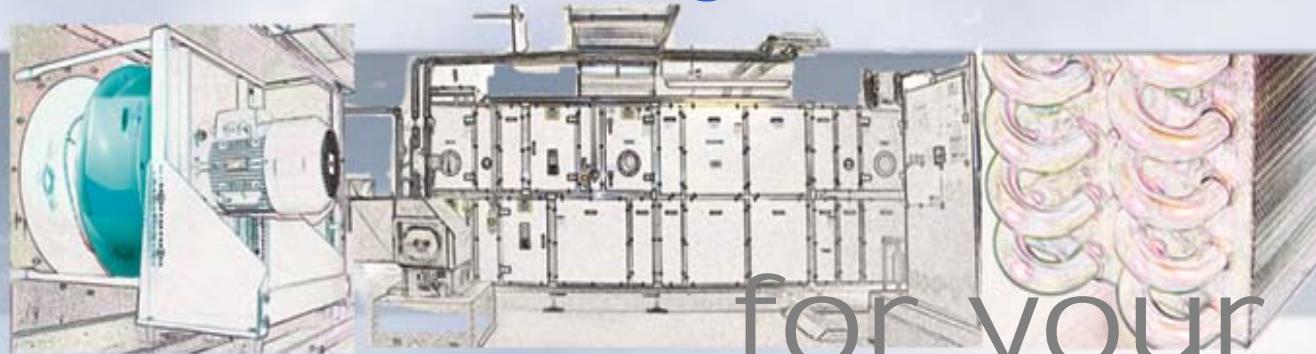
solution:

$$n_2 = (\dot{V}_2 / \dot{V}_1) \cdot n_1 = (8.000 / 10.000) \cdot 1.783 = \underline{1.426 \text{ min}^{-1}} \\ (-20,0\%)$$

$$p_{t2} = (\dot{V}_2 / \dot{V}_1)^2 \cdot p_{t1} = (8.000 / 10.000)^2 \cdot 1.200 = \underline{768 \text{ Pa}} \\ (-36,0\%)$$

$$P_2 = (\dot{V}_2 / \dot{V}_1)^3 \cdot P_1 = (8.000 / 10.000)^3 \cdot 5,7 = \underline{2,92 \text{ KW}} \\ (-48,8\%)$$

Thank you
for your
Attention



**Ventilation
energy efficiency of fans and drives
Energy recovery and energy efficiency in ventilation
technology**

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